

# Railway bridge design analysis with deck bulb tee WF98DG type bearer using bridgelink V.8.0.0.2

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## Abstract

The railroad track is crucial for people to cross the train, especially on lines with quite high elevations where the railroad is not permitted to have particularly high gridlines on its tracks. In its literal sense, a bridge is a construction that connects two areas that are divided by a barrier, which can be man-made or natural, such as highways, irrigation canals, and railroads, or it can be a river, valley, strait, or sea. The researcher will model the bridge girder with Bridgelink software for tracks on public railways, using pre-stressed concrete material with the type of girder is Deck Bulb Tee WF98DG with a bridge span of 30 m. Referring to the railway geometry planning parameters according to the Minister of Transportation regulation No. PM. 60 of 2012. From the results of this study it is known that with a bridge cross-section of 3.124 m wide according to the needs of the width of the cross-section of a one-lane railway, which is a minimum of 3 m with a span length of 30 m using a single axle load of 20 tons requires a girder cross-section type Deck Bulb Tee WF98DG with the number of straight strand recommendations from bridge link is 18 pieces and Harped Strand as many as 7 pieces using  $f_c$  35.16 MPa.

**Keywords:** Bridgelink, DeckBulbTee, Girder, Railroad, Stress.

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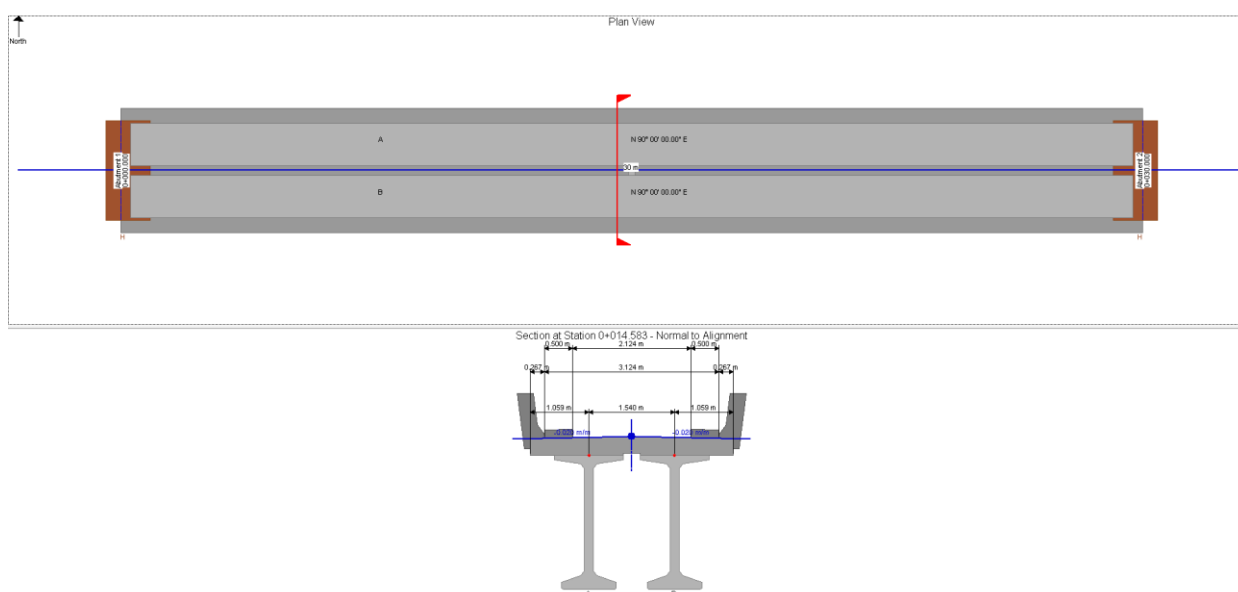
## 1. Introduction

The railroad track is crucial for people to cross the train, especially on lines with quite high elevations where the railroad is not permitted to have particularly high gridlines on its tracks. In its literal sense, a bridge is a construction that connects two areas that are divided by a barrier, which can be man-made or natural, such as highways, irrigation canals, and railroads, or it can be a river, valley, strait, or sea.

When choosing the type of bridge to use, consideration can be given to the many designs, materials, and roles that bridges have in the building industry [1]. The girder bridge offers time and cost savings, but it also has advantages and downsides depending on the materials to be utilized. The interaction between trains and bridges has become increasingly important in rail and bridge design with the development of contemporary railroads. The impact of the temperature differential on the bridge is substantial and cannot be ignored because this movement could cause the bridge to bend like a traffic load [2]. In this study, researchers carried out a numerical design of a railroad bridge using Bridgelink software where the bridge girder used was a Pretrial Girder type Deck Bulb Tee WF98DG and carried out loading with live loads on each railroad axle. By referring to the railway geometry planning parameters according to the Minister of Transportation regulation No. PM. 60 of 2012 concerning Railway Engineering Requirements, using the design boundary conditions according to the criteria used referring to the SNI 2847: 2019 standard on "Structural Concrete Requirements for Building Buildings". For prestressed flexural structural components refer to SNI 2847-2019 article 18.4.2, for prestressed flexural structural components, the stress in concrete at service load is based on the properties of the uncracked section. It is expected that this research can provide a good repertoire and contribution to the world of railways, especially in the railroad bridge section which is part of an important element in the world of railways, and provide excellent supporting data for railroad construction.

## 2. Research Method

In this study the authors will model the bridge girder with Bridgelink software for tracks on public railways, using pre-stressed concrete material with the type of grinder is Deck Bulb Tee WF98DG with a bridge span of 30 m, description as shown in Figure 1.



**Figure 1.** Typical of railroad bridges

The Regulation of the Minister of Transport of the Republic of Indonesia No. PN. 60 of 2012 on the technical standards for the railway line applies to the size of the railway bearing. The use and installation of a normal 1435mm rail width railway in a specified cant location. According to Figure 1, the rail structure is created as well as possible to be able to withstand heavy loads, or the term AXLE

LOAD, of the train series running on it. This way, the steel road can survive for a long time and the train series may travel quickly, safely, and comfortably.

## 2.1. Project Criteria

Implementing the use of the design boundary conditions by the standards established by SNI 2847: 2019 on "Structural Concrete Requirements for Building Buildings." Regarding prestressed flexural structural components, see SNI 2847-2019 article 18.4.2. The properties of the uncracked section determine the stress in the concrete at service load, as shown in figure 2.

Figure 2. General Parameter

In the checking and design within the bridge link parameters, the Harped Strand Slope Limit and Deflection limit are emphasized and designed, as shown in Figure 3.

Figure 3. Checking and Design Option

In addition, Stress Limits for temporary stresses before losses are also carried out as shown in Figure

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Stress Limits for Temporary Stresses before Losses (LRFD 5.9.4.1)

Compressive Stress   $f_c$

Tensile Stress

In areas other than the precompressed tensile zone and without bonded reinforcement   $\sqrt{f_c}$  (MPa)  But not greater than  MPa

In areas with sufficient bonded reinforcement   $\sqrt{f_c}$  (MPa)

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Stress Limits at Service Limit State after Losses (LRFD 5.9.4.2)

Compressive Stress (Effective Prestress + Permanent Loads)   $f_c$

Compressive Stress (Effective Prestress + Permanent Loads + Transient Loads)   $f_c$

Tensile Stress (Service I) (Effective Prestress + Permanent Loads = Final Stress without Live Load)   $\sqrt{f_c}$  (MPa)  But not greater than  MPa

Tensile Stress (Service III) (Effective Prestress + Permanent Loads + Transient Loads)

Not worse than moderate corrosion conditions   $\sqrt{f_c}$  (MPa)  But not greater than  MPa

Severe corrosive conditions   $\sqrt{f_c}$  (MPa)  But not greater than  MPa

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Stress limit for Fatigue (LRFD 5.5.3.1)

Fatigue I plus one-half the sum of effective prestress and permanent   $f_c$

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Stress Limits for Temporary Loading Conditions (PGSuper Only)

Evaluate stress limits for temporary loading conditions

Stress Limits immediately after Temporary Strand Removal

Compressive Stress   $f_c$

Tensile Stress in areas other than the precompressed tensile zone

$\sqrt{f_c}$  (MPa)  But not greater than  MPa

In areas with sufficient bonded reinforcement   $\sqrt{f_c}$  (MPa)

Stress Limits immediately after Deck Placement

Compressive Stress   $f_c$

Tensile Stress   $\sqrt{f_c}$  (MPa)  But not greater than  MPa

Figure 4. Stress Limits

Prestressing stress limit conditions also adjusts SNI 2847-2019, as shown in Figure 5.

Stress Limits for Prestressing (5.9.3)

Check at Jacking

Stress Relieved Strands  fpu

Low Relaxation Strands  fpu

Check Immediately Prior to Transfer

Stress Relieved Strands  fpu

Low Relaxation Strands  fpu

Check After Transfer

Stress Relieved Strands  fpu

Low Relaxation Strands  fpu

After all losses

Stress Relieved Strands  fpu

Low Relaxation Strands  fpu

Pretensioned Strand Options

Allow Extended Straight Strands

Compute the transfer length of prestressing strands using the following method:

Size of Ducts (LRFD 5.4.6.2)

Minimum ratio of inside area of duct to net area of prestressing steel

for strands placed by the push method

for strands placed by the pull-through method

Outside diameter of duct shall not exceed  times the least gross concrete thickness at the duct

Stress Limits for Post-tensioning (5.9.3)

Check at Jacking

Stress Relieved Strands  fpu

Low Relaxation Strands  fpu

Check prior to seating

Stress Relieved Strands  fpu

Low Relaxation Strands  fpu

At anchorages and couples immediately after anchor set

Stress Relieved Strands  fpu

Low Relaxation Strands  fpu

Elsewhere along length of member away from anchorages at anchor set

Stress Relieved Strands  fpu

Low Relaxation Strands  fpu

After all losses

Stress Relieved Strands  fpu

Low Relaxation Strands  fpu

Figure 5. Prestressing stress limit

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In the analysis process, design checks and recommendations are carried out by determining the boundary conditions and warning design boundary conditions shown in Figure 6.

Warnings will be posted to the Status Center if the following limits are exceeded.

**General Warnings**

Warn if stirrup zone lengths are incompatible with stirrup spacings

Warn if there is a potential for girders to sag under dead load effects

Base sag detection on

**Concrete Limits**

|                      | Normal Weight             | Lightweight               |
|----------------------|---------------------------|---------------------------|
| Deck                 | 41.37 MPa                 | 41.37 MPa                 |
| Precast Element f'ci | 51.71 MPa                 | 51.71 MPa                 |
| Precast Element f'c  | 68.95 MPa                 | 62.05 MPa                 |
| Closure Joint f'ci   | 41.37 MPa                 | 41.37 MPa                 |
| Closure Joint f'c    | 55.16 MPa                 | 55.16 MPa                 |
| Concrete Unit Weight | 2643.05 kg/m <sup>3</sup> | 2002.31 kg/m <sup>3</sup> |
| Max Aggregate Size   | 38.1 mm                   | 38.1 mm                   |

**Figure 6.** Warning recommendation design

## 2.2. Load

The available load cases for defining a load are DW (dead load, worn surface), LL+IM (live load plus impact), and DC (dead load, component). Assuming that the sidewalk and rail are situated at the edge of the slab, PGSuper models this situation by dividing the live loads of the sidewalk, rail, and pedestrian evenly among the three external beams. On the other hand, 1/3 of the rail weight is applied to the first inside beam and 2/3 to the external beam when modeling U beams. You can set the rail to "none" and add the rail load using the "Add Distributed Load" tool in "User Defined Loads" if you'd want to distribute the weight differently. Anyone can choose which vehicle to utilize for Service and Strength Limit States, Fatigue Limit States, and Permit Limit States using this application. HL-93, the Fatigue truck, and no truck are the default options.

PGSuper will activate the Pedestrian on Sidewalk load immediately if you model a sidewalk. PGSuper will automatically enclose both the vehicle and sidewalk live loads by default. Unchecking the box next to the load case will disable the pedestrian live load. To determine whether loading vehicular and pedestrian live load, vehicular only, or pedestrian solely is best suited for the design, engineering judgment, and experience should be employed.

The AASHTO LRFD Bridge Design Specifications' Section 4.6.2.2 contains the Ranges of Applicability (ROA), which are limits on the research that was done on distribution factors. The range for which the formulas are valid is not always indicated by the ROA; rather, they reflect the boundaries of the research that was done to develop the formulas. It is up to the engineer's discretion to determine whether to use the formulas or find the live load distribution factor using an alternative method when a design is outside the ROA. An engineer could first ascertain how sensitive the formula in question is to the relevant variable to help with this decision. When using 8 Axles, Standard Axle Spacing for Steam Locomotives is The heaviest plus the coal train has a total load of 168 tonnes or 8.75 tonnes/m<sup>2</sup>[1], [3].

In this study, the earthquake load was carried out by simulating the area in earthquake region 3 with a base shear coefficient of 0.15 with medium soil conditions. The rail structure is made as best as possible to be able to withstand heavy loads, in this study using the weight of one train axle by the

Regulation of the Minister of Transportation of the Republic of Indonesia No. 60 of 2012 concerning technical standards for railroad tracks applicable to simulating loading on railroad tracks, from a series of trains running on it. Thus, the steel road can last a long time and trains can travel quickly, safely, and comfortably.

**Table 1.** User Define Loads

| Type    | Event                         | Load Case | Location                                | Magnitude |
|---------|-------------------------------|-----------|-----------------------------------------|-----------|
| Point   | Event 7: Final with Live Load | LL + IM   | Span 1, All Girders, 50%                | 200.00 Kn |
| Uniform | Event 4: Cast Deck            | DW        | All Spans, All Girders, the Entire Span | 1,15 kN/m |
| Uniform | Event 4: Cast Deck            | DC        | All Spans, All Girders, the Entire Span | 1,03 kN/m |
| Uniform | Event 7: Final with Live Load | LL + IM   | All Spans, All Girders, the Entire Span | 1,01 kN/m |
| Uniform | Event 7: Final with Live Load | LL + IM   | All Spans, All Girders, the Entire Span | 0,49 kN/m |
| Uniform | Event 7: Final with Live Load | LL + IM   | All Spans, All Girders, the Entire Span | 2,23 kN/m |

In this study, the factored load adjusts the loading combination based on SNI 1725: 2016 concerning Loading for Bridges shown in Figure 7, and is used as a parameter in the analysis in Bridgeline according to Table 2.

**Table 2.** Load combination based on SNI 1725: 2016

| Keadaan Batas     | MS         | TT            | EU   | EW <sub>s</sub> | EW <sub>L</sub> | BF   | EUn       | TG            | ES            | Gunakan salah satu |      |      |    |
|-------------------|------------|---------------|------|-----------------|-----------------|------|-----------|---------------|---------------|--------------------|------|------|----|
|                   | MA         |               |      |                 |                 |      |           |               |               | TD                 | EQ   | TC   | TV |
|                   | TA         |               |      |                 |                 |      |           |               |               | TB                 |      |      |    |
|                   | PR         |               |      |                 |                 |      |           |               |               | TP                 |      |      |    |
|                   | PL         |               |      |                 |                 |      |           |               |               |                    |      |      |    |
|                   | SH         |               |      |                 |                 |      |           |               |               |                    |      |      |    |
| Kuat I            | $\gamma_P$ | 1,8           | 1,00 | -               | -               | 1,00 | 0,50/1,20 | $\gamma_{TG}$ | $\gamma_{ES}$ | -                  | -    | -    |    |
| Kuat II           | $\gamma_P$ | 1,4           | 1,00 | -               | -               | 1,00 | 0,50/1,20 | $\gamma_{TG}$ | $\gamma_{ES}$ | -                  | -    | -    |    |
| Kuat III          | $\gamma_P$ | -             | 1,00 | 1,40            | -               | 1,00 | 0,50/1,20 | $\gamma_{TG}$ | $\gamma_{ES}$ | -                  | -    | -    |    |
| Kuat IV           | $\gamma_P$ | -             | 1,00 | -               | -               | 1,00 | 0,50/1,20 | -             | -             | -                  | -    | -    |    |
| Kuat V            | $\gamma_P$ | -             | 1,00 | 0,40            | 1,00            | 1,00 | 0,50/1,20 | $\gamma_{TG}$ | $\gamma_{ES}$ | -                  | -    | -    |    |
| Ekstrem I         | $\gamma_P$ | $\gamma_{EQ}$ | 1,00 | -               | -               | 1,00 | -         | -             | -             | 1,00               | -    | -    |    |
| Ekstrem II        | $\gamma_P$ | 0,5           | 1,00 | -               | -               | 1,00 | -         | -             | -             | -                  | 1,00 | 1,00 |    |
| Daya Layan I      | 1,00       | 1,00          | 1,00 | 0,30            | 1,00            | 1,00 | 1,00/1,20 | $\gamma_{TG}$ | $\gamma_{ES}$ | -                  | -    | -    |    |
| Daya Layan II     | 1,00       | 1,30          | 1,00 | -               | -               | 1,00 | 1,00/1,20 | -             | -             | -                  | -    | -    |    |
| Daya Layan III    | 1,00       | 0,80          | 1,00 | -               | -               | 1,00 | 1,00/1,20 | $\gamma_{TG}$ | $\gamma_{ES}$ | -                  | -    | -    |    |
| Daya Layan IV     | 1,00       | -             | 1,00 | 0,70            | -               | 1,00 | 1,00/1,20 | -             | -             | -                  | -    | -    |    |
| Fatik (TD dan TR) | -          | 0,75          | -    | -               | -               | -    | -         | -             | -             | -                  | -    | -    |    |

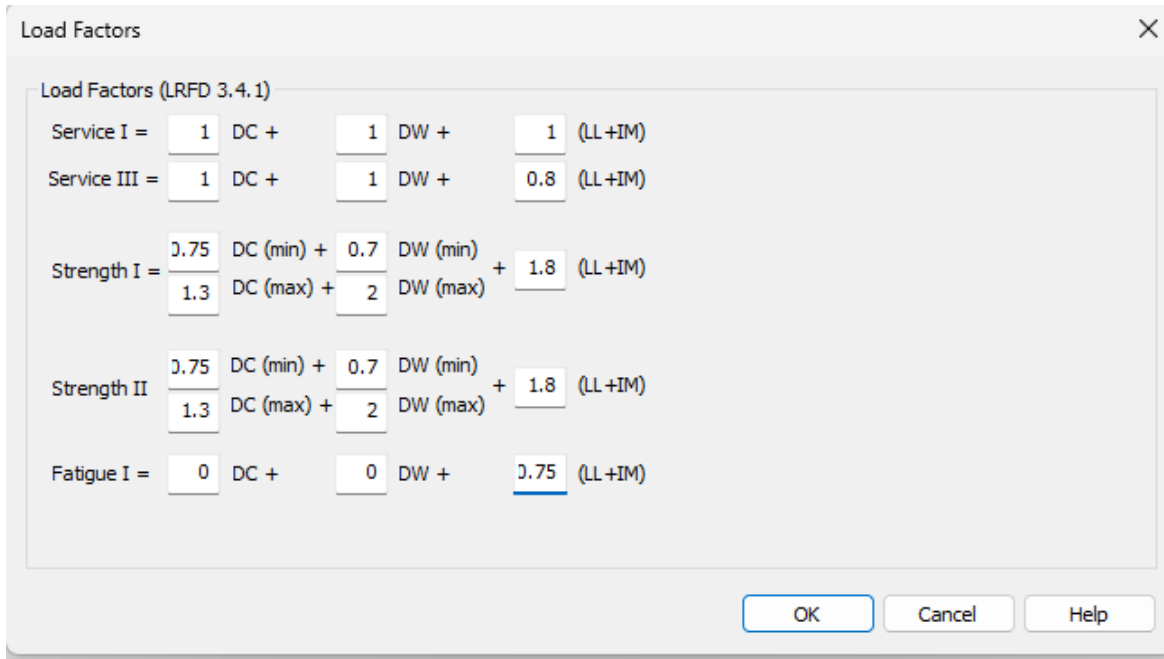


Figure 7. Load combination on Bridgeline

## 2.3. Rail

A. Rails must adhere to the following standards:

1. 10% or more of an elongation;
2. at least 1175 N/mm<sup>2</sup> in terms of tensile strength;
3. The rail head's hardness shouldn't be less than 320 BHN.

The rail cross-section needs to match the rail measurements, as shown in the chart and the image below.

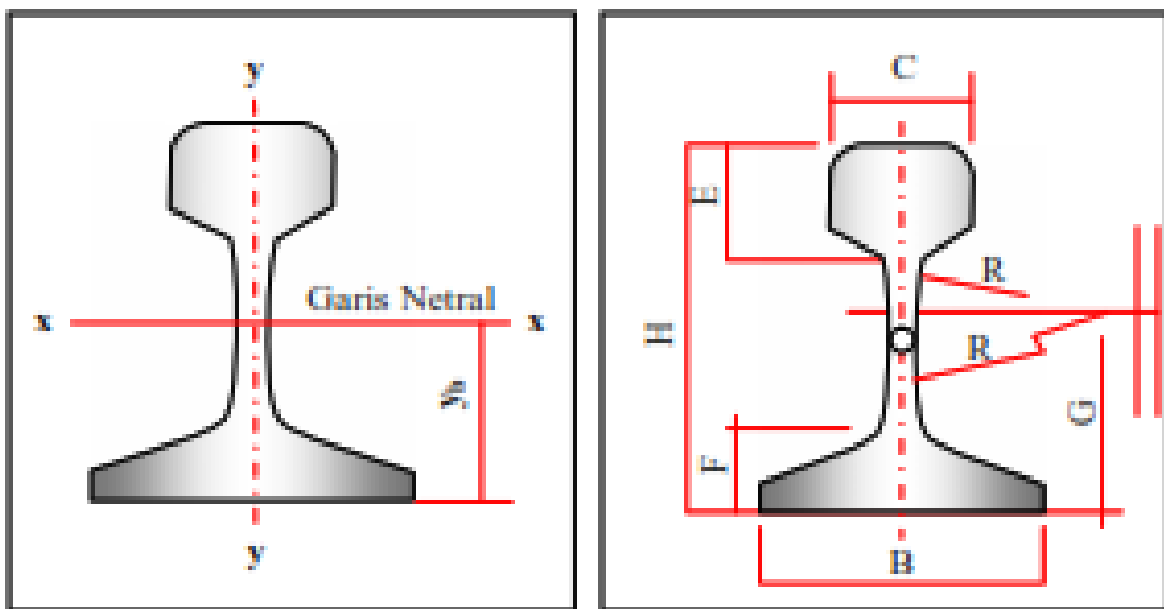


Figure 10. Rail dimensions

The different types of rail rods have an impact on both the maximum pressure (axle load) the rail can withstand during a train pass and the maximum speed of the train as it passes the rail. With an increase

in "R," the axle load that the rail can support increases, enabling trains to cross it safely and steadily at high speeds.[4].

**Table 3.** Rail Section Dimensions

| Geometric size                    | Rail Type |          |          |          |
|-----------------------------------|-----------|----------|----------|----------|
|                                   | R 42      | R 50     | R 54     | R 60     |
| H (mm)                            | 138.00    | 153.00   | 159.00   | 172.00   |
| B (mm)                            | 110.00    | 127.00   | 140.00   | 150.00   |
| C (mm)                            | 68.50     | 65.00    | 70.00    | 74.30    |
| D (mm)                            | 13.50     | 15.00    | 16.00    | 16.50    |
| E (mm)                            | 40.50     | 49.00    | 49.40    | 51.00    |
| F (mm)                            | 23.50     | 30.00    | 30.20    | 31.50    |
| G (mm)                            | 72.00     | 76.00    | 74.79    | 80.95    |
| R (mm)                            | 320.00    | 500.00   | 508.00   | 120.00   |
| A (cm <sup>2</sup> )              | 54.26     | 64.20    | 69.34    | 76.86    |
| W (kg/m)                          | 42.59     | 50.40    | 54.43    | 60.34    |
| I <sub>x</sub> (cm <sup>4</sup> ) | 1,369.00  | 1,960.00 | 2,346.00 | 3,055.00 |
| Y <sub>b</sub> (mm)               | 68.50     | 71.60    | 76.20    | 80.95    |

The explanation of the symbol above is

A = cross-sectional area

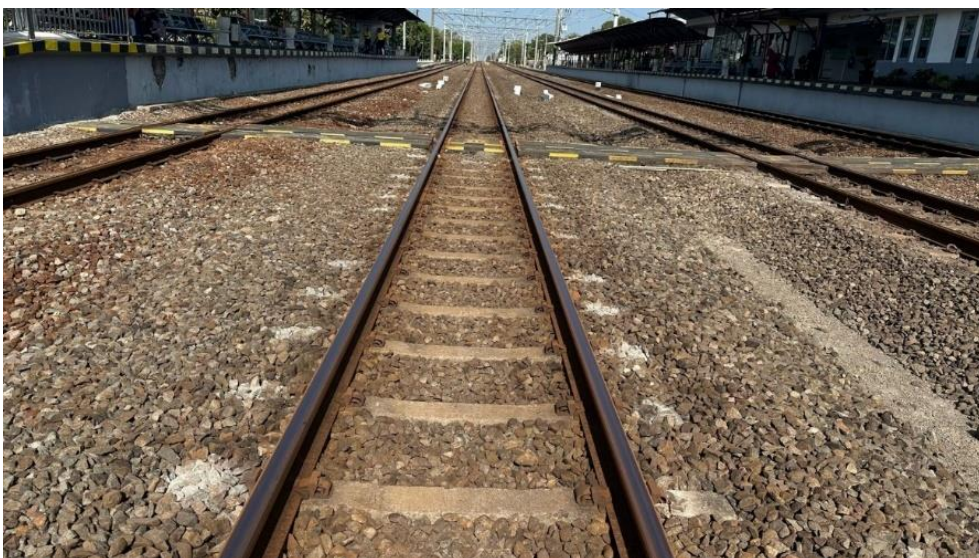
W = rail weight per meter

I<sub>x</sub> = moment of inertia about the x-axis

Y<sub>b</sub> = the distance from the bottom of the rail to the neutral line

## 2.4. Railway components

After the foundation layer is completed as the foundation of the railway, the next stage is to build the railway tracks. Please note that each component affects the quality of the railway itself. Figure 8 below shows a railroad schematic and its components.



**Figure 8.** Railroad track components

## 2.5. Fenite element Method (FEM)

The finite element method (FEM) is a mathematical strategy used to deal with specific evaluation problems. The limited component approach combines a few numerical concepts to generate straight or nonlinear framework conditions. The number of conditions produced is usually extremely large, exceeding 20,000 conditions. As a result, unless a decent PC is used, this approach is of little practical value.

When a design is subjected to forces such as stress, pressure, temperature, stream rate, and severity, the result is strain (distortion), stress, temperature, tension, and stream rate. The concept of the following action (twisting) on a body is based on the characteristics of the power and stress structure itself. The dissemination of this effect, conveyed as dislodging, can be tracked down in the limited component approach.

To deal with the problem of tracking down relocations of vertices/associations/grids and primary powers, the finite element technique employs a component discretization method. Discrete component conditions are linked with the lattice method for initial examination, and the results obtained are indistinguishable from those obtained from conventional structural inquiry. Discreteness should be achievable using one-layered components (line components), two-layered components (planar components), or three-layered components (volume/continuum components). This method employs a continuous component to determine a more accurate response.[5], [6], [7], [8], [9], [10], [11], [12], [13], [14], [15], [16], [17], [18].

## 2.6. Bridgeline-PGSuper

BridgeLink™ is an integrated suite of bridge engineering software. BridgeLink™ links together several different bridge engineering software tools into one convenient and easy-to-use platform.

BridgeLink™ currently supports the following software tools:

1. Barlist™ - Reinforcing steel quantity estimating tool
2. BEToolbox™ - Bridge Engineering Toolbox utility programs
3. PGSplice™ - Precast-Prestressed Spliced Girder Design, Analysis, and Load Rating
4. PGSuper™ - Precast-Prestressed Girder Design, Analysis, and Load Rating
5. TOGA™ - TxDOT Optional Girder Analysis tool
6. XBRate™ - Reinforced Concrete Cross Beam Load Rating

Precast-Prestressed Girder design, analysis, and load rating software is called PGSuper™. Precast-prestressed girder bridges can be designed, verified, and loaded according to DOT agency-specific requirements and the AASHTO LRFD Bridge Design Specification using PGSuper™. The minimum necessary concrete release strength as well as the quantity and arrangement of prestressing strands are calculated by the flexural design feature. For vertical shear, horizontal shear, bursting, and strand confinement, the number, size, and spacing of transverse reinforcement are determined by the shear design feature. Girders are assessed for compliance with strength, service, and detailing criteria through specification checking. Girders are assessed for stability and stress while being handled and transported. It is also possible to use temporary prestressing to reduce concrete release strengths, enhance stability, and control camber.

This software has taken into consideration the limitations and capabilities of local fabricators. Because of its adaptable design, PGSuper™ can be expanded upon and updated in the future as user demands and design specifications shift[19], [20], [20], [21].

## 3. Results And Discussion

In this study, researchers used 1 axle with a standard axle spacing with a load of 20 tons. The largest axle load plan suitable for operating rolling stock, or load plan scheme, is the live load used. The load plan scheme 1921 (RM 21) can be applied to axle loads up to 20 tons. The axle load on which the planning process is based should be by the route classification and the maximum load of the operating rolling stock, while the materials used in modeling are as follows.

### 3.1. Section Parameters

The girder type used is a pre-stressed girder of the Deck Bulb Tee WF98DG type with an upper wingspan of 1540 mm and a height of 2476.5 mm, as shown in Figure 9 with some detailed parameters as shown in Figure 10 with a bridge span of 30 m.

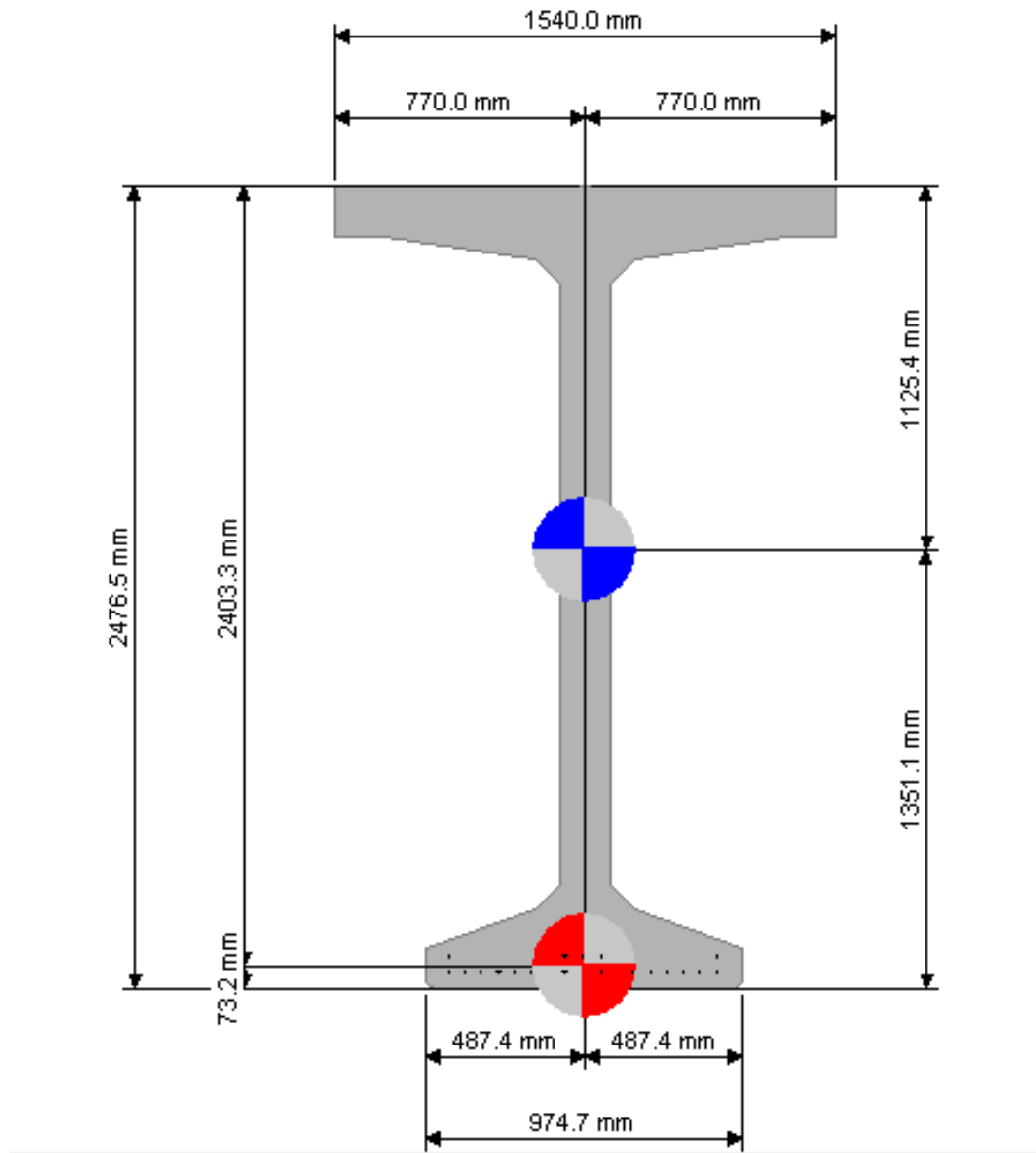


Figure 9. Typical Deck Bulb Tee WF98DG girder type dimensions

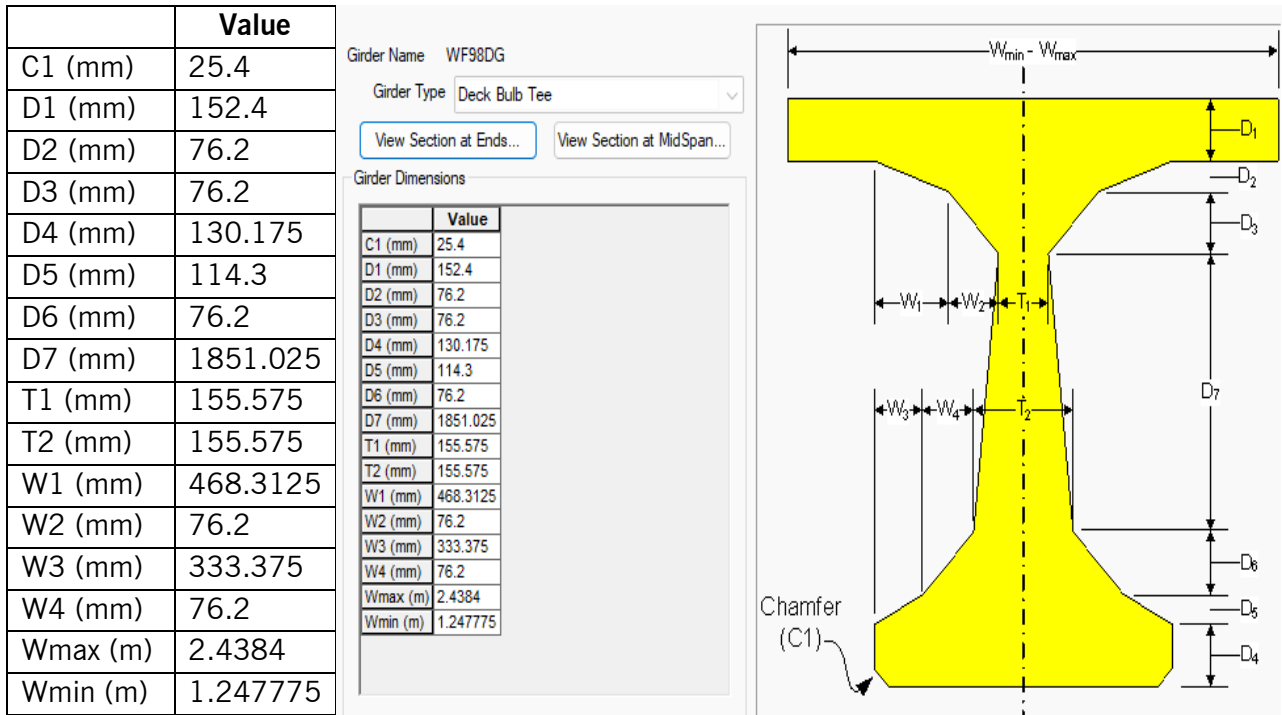


Figure 10. Section of Deck Bulb Tee WF98DG girder

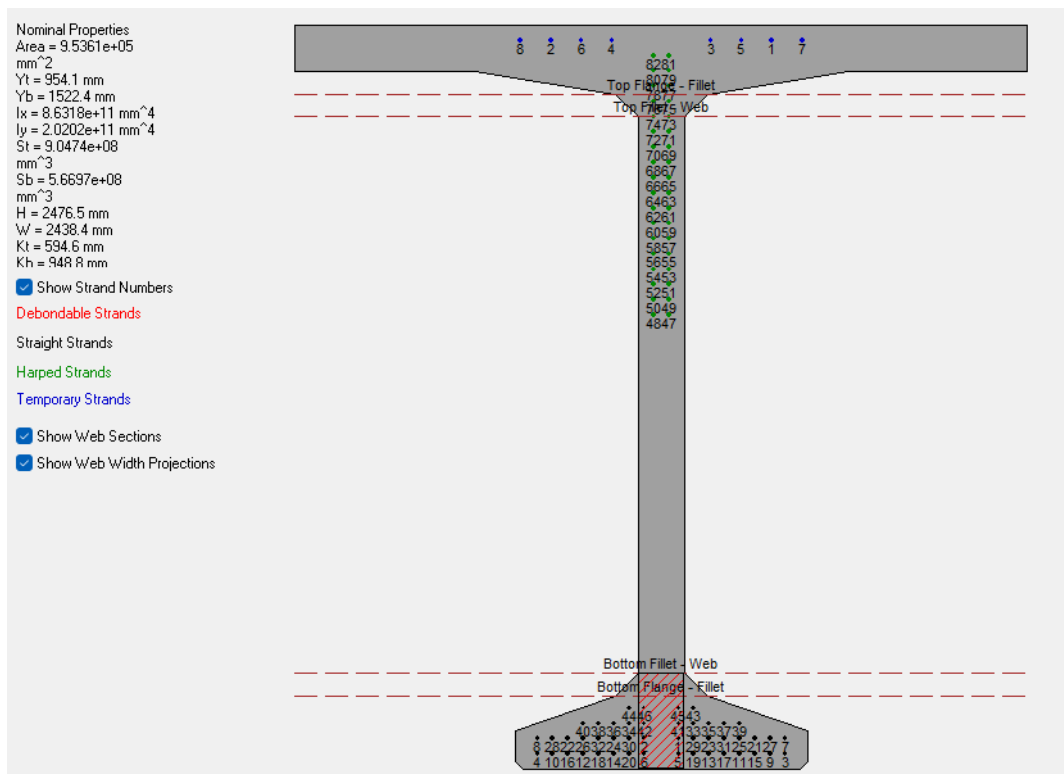
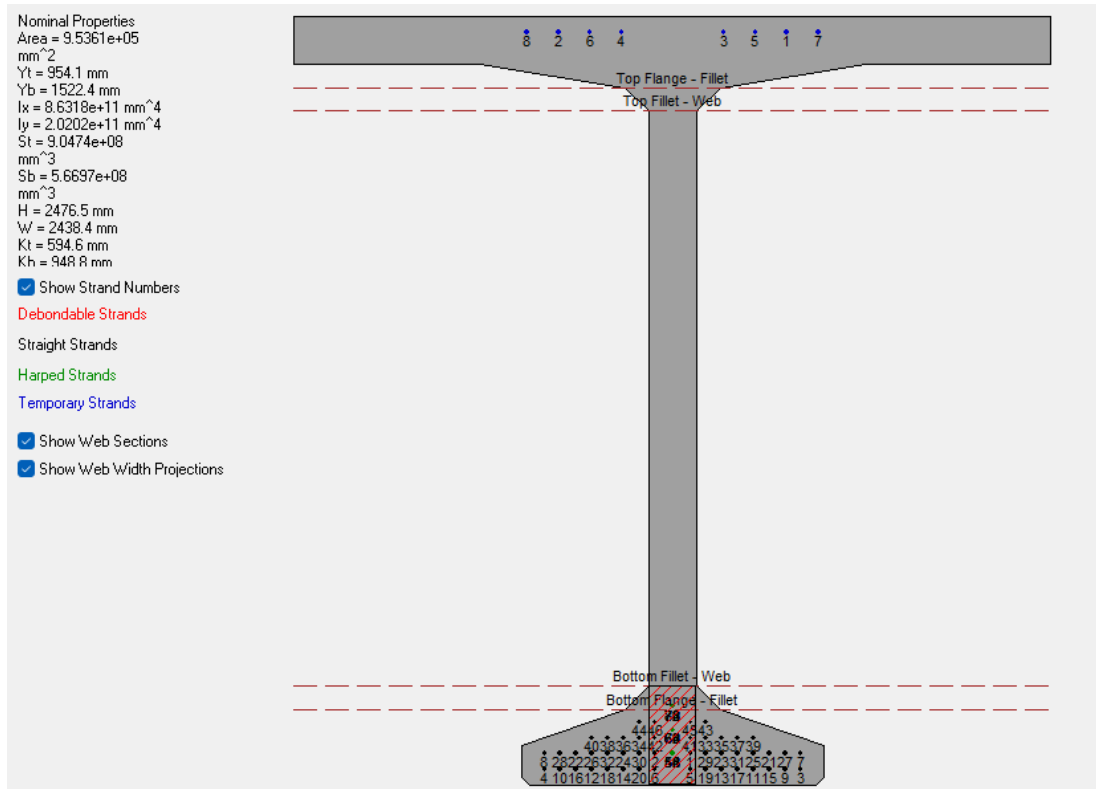


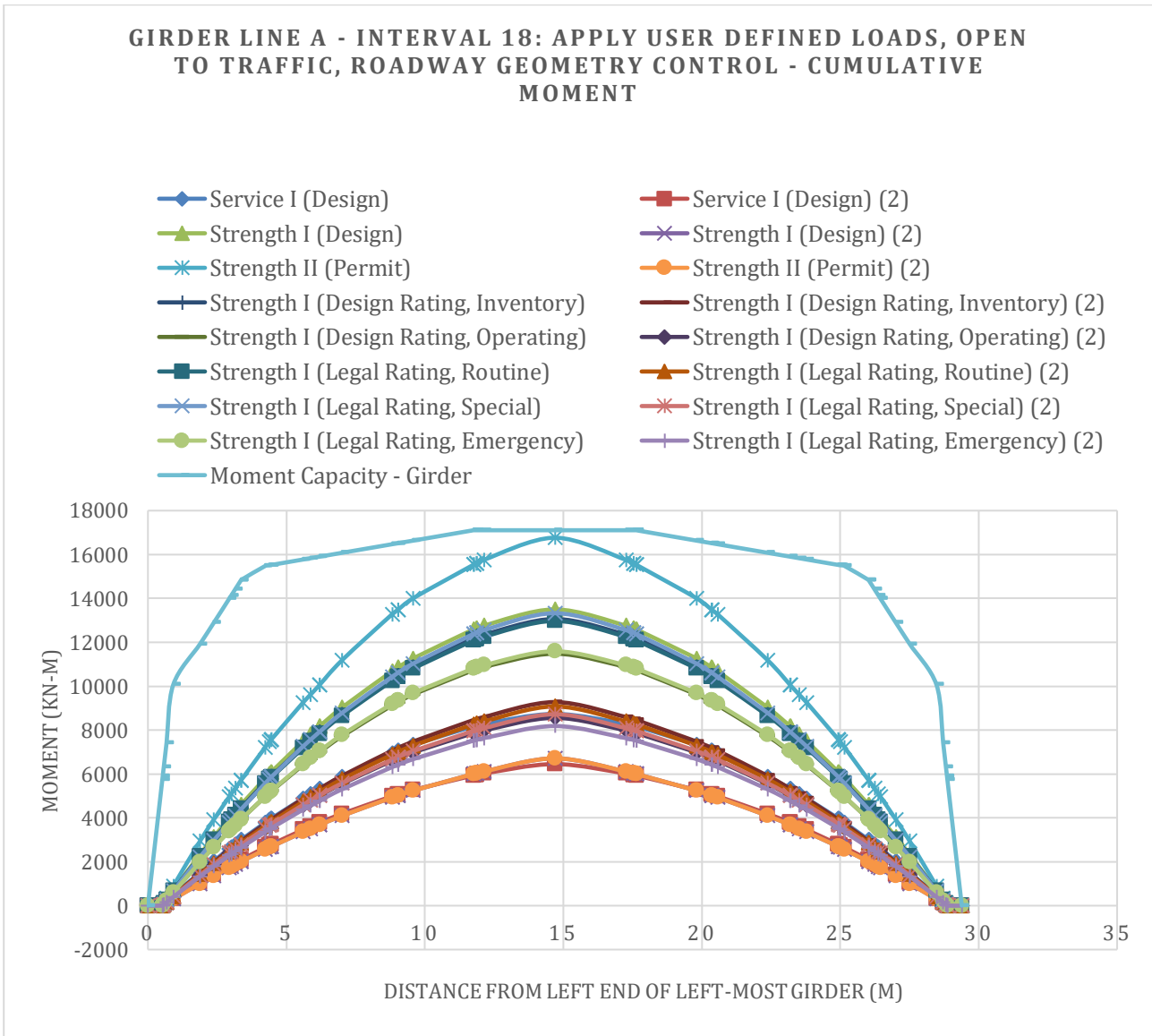
Figure 11. End Section of Deck Bulb Tee WF98DG girder

The strand arrangement formation on the girder used for the girder end position is as shown in Figure 11 and the position at the middle of the girder is as shown in Figure 12.



### 3.2. Bridgelink Design Analysis

One of the results issued by the analysis using Bridgelink is the moment capacity, shown in Figure 14, where the moment capacity of the girder used is the light green line marked with a yellow arrow, indicating the ability of the girder is still greater than the forces that occur due to several conditions that have been described in Figure 7, which confirms that these conditions are still below the condition of the girder element capabilities that have been designed and used as research parameters.



**Figure 14.** Moments that occur along the span and some conditions due to the forces that occur

Table 4 describes the output results and recommendations from Bridgelink in analyzing the capabilities of the elements when first entered, Bridgelink provides ideal recommendations in planning by providing options for adding strands, strand positions, and providing options for increasing the quality of concrete used ideally, Figure 18 provides information from the initial design results, namely the current value and recommendations given according to the proposed design column.

**Table 4.** Analysis output table and design recommendations by bridge link

| Parameter                                                                                | Proposed Design | Current Value |
|------------------------------------------------------------------------------------------|-----------------|---------------|
| Number of Straight Strands                                                               | 18              | 18            |
| Number of Harped Strands                                                                 | 7               | 7             |
| Number of Temporary Strands                                                              | 0               | 0             |
| Straight Strand Jacking Force                                                            | 3518.39         | 3518.39       |
| Harped Strand Jacking Force                                                              | 1368.26         | 1368.26       |
| Temporary Strand Jacking Force                                                           | 0.00 Kn         | 0.00 Kn       |
| Distance from bottom of girder to bottom of harped strand group at start of girder       | 1409.7 mm       | 1409.7 mm     |
| Distance from bottom of the girder to bottom of harped strand group at end of the girder | 1409.7 mm       | 1409.7 mm     |
| Distance from bottom of girder to bottom of harped strand group at left of girder        | 101.6 mm        | 101.6 mm      |
| Distance from bottom of girder to bottom of harped strand group at right of girder       | 101.6 mm        | 101.6 mm      |
| Eccentricity of Permanent Strands at Midspan                                             | 1276.9 mm       | 1276.9 mm     |
| $f'_{ci}$                                                                                | 31.72 MPa       | 31.72 MPa     |
| $f'_c$                                                                                   | 35.16 MPa       | 35.16 MPa     |
| Slab Offset ("A" Dimension)                                                              | 365.4 mm        | 365.4 mm      |

Concrete release strength was controlled by flexural stress in Interval 2 Prestress Release, Service I, Compression, at the Bottom of the Girder. Concrete final strength was controlled by flexural stress in Interval 18 Apply User Defined Loads, Open to Traffic, Roadway Geometry Control, Service I, Compression, at the Bottom of Girder.

#### 4. Conclusion

From the results of the analysis of this study, it is known that with a bridge cross-section of 3.124 m wide according to the needs of the width of the cross-section of a one-lane railway, which is a minimum of 3 m with a span length of 30 m using a single axle load of 20 tons requires a girder cross-section type Deck Bulb Tee WF98DG with the number of straight strand recommendations from bridge link is 18 pieces and Harped Strand as many as 7 pieces using  $f'_c$  35.16 MPa. This research needs to be continued because in this study using girders with types that already exist in Bridgelink's design criteria, further research should design with other cross-sectional dimensions according to local needs, to provide information and facilitate work and finding girder dimensions and some very broad options to be reviewed.

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